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14. ABSTRACT						
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-Monolithic Al5083	iii Oii.					
-Baseline						
-Proposed seam design of thickened edges						
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15. SUBJECT TERMS						
	Adhesive Layer Effect, .30cal AP M2 Projectile, 762x39 PS Projectile, SPH, Aluminum 5083, SiC, DoP Expeminets, AutoDyn Si					
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PROGRESS REPORT
March 2014

Nicole A. Cicchetti, Bazle Z. (Gama) Haque, Shridhar Yarlagadda, John W. Gillespie Jr.

MODELING AND SIMULATION OF CERAMIC ARRAYS TO IMPROVE BALLISTIC PERFORMANCE

TECHNICAL APPROACH



The University of Delaware Center for Composite Materials (UD-CCM) is developing the next generation of lightweight hybrid ceramic/composite armor kits for Marine Corps tactical and combat vehicles The focus is on simulating and modeling the performance of ceramic/composite lightweight armor at seams and corners, and improving the armor's performance in these regions The ceramic/composite armor is comprised of composite backings, adhesives, ceramics and covers The tiles will be restricted to the sintered ceramics (SiC) due to the ability to fabricate SiC into complex geometries and cost analysis conducted in previous research Model ballistic experiments will validate the modeling done in simulation

TECHNICAL APPROACH

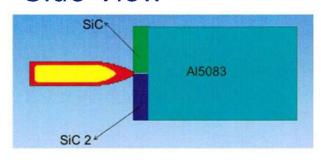


Half-symmetric model is used in AutoDyn to simulate Depth of Penetration (DOP) experiments on SiC tile with and without a gap supported by solid Aluminum (Al5083) Impacts by .30cal AP-M2 projectile and are modeled using SPH elements in AutoDyn Center strike model validation runs with SiC tiles are conducted based on the DOP experiments described in reference - ARL-TR-2219, 2000 Tile gap is found to increase the DOP as compared to baseline center impact Simulations were run on gap sizes 0.508 (20 mil) and 1.061 mm (40 mil) at the standard muzzle speed of 850 m/s DOP is the main measurement used to determine which geometry and configuration yield the best results.

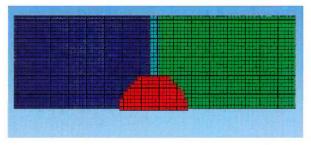
TECHNICAL APPROACH, MODEL SET UP



Side View



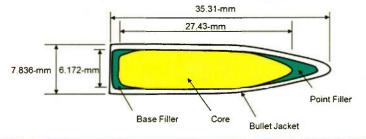
Front View



- □ Smoothed-particle
 hydrodynamics (SPH) used
 for all parts, SPH Size = 0.2
- ☐ SiC and SiC 2 are identical in properties and dimensions
 - ☐ Differentiated to show damage in each tile
- Clamp boundary condition used

Material Models MATERIAL EOS STRENGTH MODEL FAILURE MODEL Steel Core Polynomial Johnson & Cook Johnson & Cook Lead Filler Gruneisen Piecewise Johnson & Cook N/A Copper Jacket Linear Piecewise Johnson & Cook N/A SIC Ceramic JH-2 JH-2 Polynomial Aluminum Polynomial Johnson & Cook Johnson & Cook S-Glass/Phenolic Linear LS-DYNA MAT162 LS-DYNA MAT162 Polymeric Foam Linear Non-linear Elastic N/A Adhesives & Interlayers N/A Cohesive Laws Cohesive Laws

.30cal AP-M2 Projectile

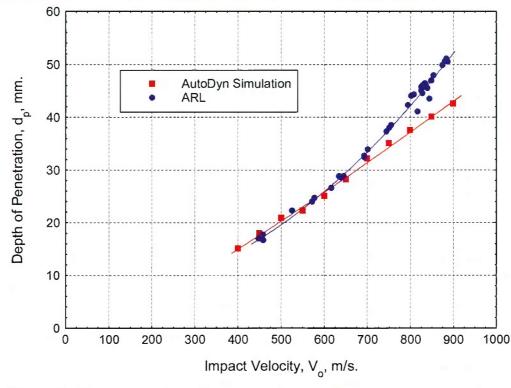


Component	Material	Weight (g)	
Jacket	Gilding Metal	4.2	
Core	Hardened Steel - RC 63	5.3	
Point Filler	Lead	0.8	
Base Filler	Lead	0.5	
Total Weight		10.8	

MONOLITHIC AI5083 DOP AT SPH SIZE 0.2 COMPARED WITH ARL DATA



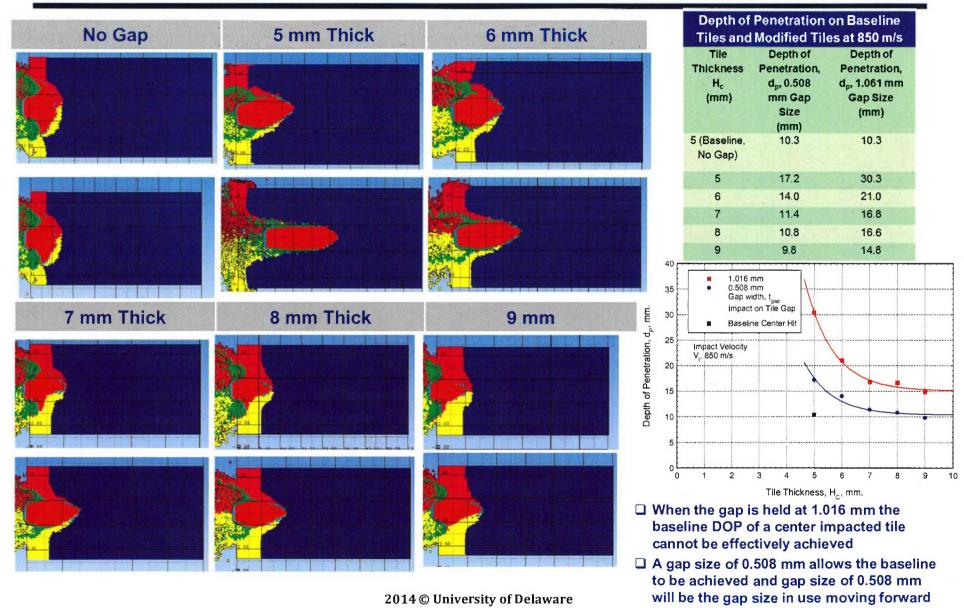
Monolithic Al5083 DOP				
Velocity (m/s)	DOP (mm)			
400	15.0			
450	17.9			
500	20.8			
550	22.2			
600	25.0			
650	28.1			
700	32.1			
750	35.0			
800	37.5			
850	40.0			
900	42.5			



- I Simulation results do not show the same trend as the ARL experimental data
- Simulations will be extended over a larger range of Impact Velocities
- Material properties may be edited if the properties do not match the material properties used in the ARL experiments

EFFECT OF TILE THICKNESS ON DOP AT 850m/s **GAP SIZE 0.508**mm **AND 1.016**mm

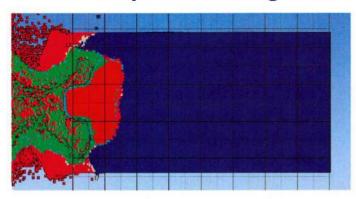




ADHESIVE LAYER EFFECT



Center Impacted Single Tile



Adhesive Layer DOP Compared to No Adhesive Layer DOP, Gap 0.508 mm Adhesive Layer DOP Baseline Center (mm) Impact with no Adhesive DOP (mm)

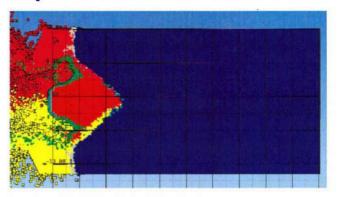
10.1

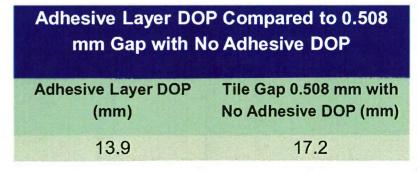
An adhesive layer of Epoxy
 Resin was added in between the
 SiC tile and the Al backing

10.3

☐ The tile remained 5 mm thick

Impact on a Tile with 0.508 mm Gap



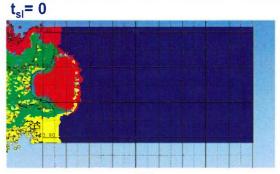


- An adhesive layer of Epoxy Resin was added in between the SiC tile and the Al backing
- ☐ The tile remained 5 mm thick and the gap size at 0.508 mm to compare when no adhesive was added

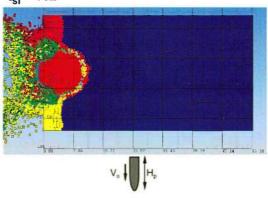
STEP LADDER SEAM DESIGN

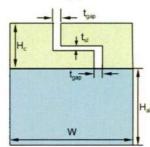


CENTER IMPACTED STEP LADDER



CENTER IMPACTED STEP LADDER t_{sl} = 0.2





Part			
Vo	850 m/s	t _{sl}	0 mm
H _p	35.31 mm	H _{al}	50 mm
t _{gap}	0.508 mm	W	30 mm
H _c	5 mm		

Part			
V _o	850 m/s	t _{si}	0.2 mm
H _p	35.31 mm	H _{al}	50 mm
t _{gap}	0.508 mm	W	30 mm
H _c	5 mm		

2014 © University of Delaware

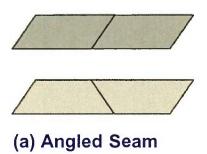
Step Ladder DOP					
Step Ladder t _{sl} = 0 mm DOP (mm)	Step Ladder t _{sl} = 0.2 mm DOP (mm)	No Step Ladder DOP, Gap Size 0.508 mm (mm)	Baseline Center Impacted One Tile		
9.2	11.8	17.2	10.3		

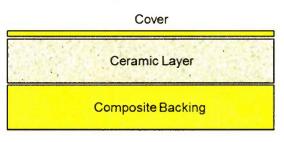
- □ An Step Ladders were created according to the schematics with presented specifications
 - The tile remained 5 mm thick and the gap size at 0.508 mm to compare to the baseline results
- ☐ The DOP results are compare against center impacted single tile and standard 0.508 mm gap between two tiles

FUTURE WORK



- Angled Seams (a) and Cover plates (b) are proposed seam designs to be tested in the future
- □ Continued modeling and experimental tests will down select for the best solution and improvement to seam design
- Modeling will move from AutoDyn to LS-DYNA for increased computational power and the ability to model complex geometries





(b) Cover Plate

SUMMARY



Simulations were run on: Monolithic Al5083 Baseline Proposed seam design of thickened edges Inefficient solution Ceramic tiles with and without gap with the adhesive layer modeled AutoDyn accurately models the behavior of the adhesive Proposed seam design of step ladder Reasonable possible solution AutoDyn material properties may need to be adjusted to capture the full damage that is occurring Future work will include new seem designs, experimental testing and modeling done in LS-DYNA